Continuous observer design for nonlinear systems with sampled and delayed output measurements

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Abstract: We design observers for nonlinear systems with sampled and delayed output measurements. The observers are of continuous and hybrid in nature. Based on an auxiliary integral technique, the exponential stability of the estimation errors is achieved, and the sampling period and the maximum delay are also given. Finally, numerical examples are provided to illustrate the design methods.

1. INTRODUCTION

In this paper, we consider the following system

\[
\begin{align*}
\dot{x}_1(t) &= x_2(t) + f_1(x_1(t)), \\
\dot{x}_2(t) &= x_3(t) + f_2(x_1(t), x_2(t)), \\
&\vdots \\
\dot{x}_{n-1}(t) &= x_n(t) + f_{n-1}(x_1(t), x_2(t), \ldots, x_{n-1}(t)), \\
\dot{x}_n(t) &= f_n(x_1(t), x_2(t), \ldots, x_n(t)) + u(t), \\
y(t) &= x_1(t),
\end{align*}
\]

(1)

where the state \( x(t) \in \mathbb{R}^n \), the input \( u(t) \in \mathbb{R} \). We assume that the output \( y(t) \) is sampled at instants \( t_k \) and is available for the observer at instants \( t_k + \tau_k \), where \( \{\tau_k\} \) denotes a strictly increasing sequence such that \( \lim_{k \to \infty} \tau_k = \infty \) and \( \tau_k \geq 0 \) represents the transmission delay. The sampling interval \( T = t_{k+1} - t_k \) is a positive constant. The transmission delays \( \tau_k \) are unknown, but have an upper bound \( \bar{\tau} \), that is, \( \max\{\tau_k\} \leq \bar{\tau} \) for all \( k = 0, 1, \ldots, \infty \). We also make the assumption: \( \bar{\tau} < T \), that is, the measures sampled at instants \( t_k \) are available for the observer before the next measures sampled at instants \( t_{k+1} \). In addition, \( f_i() \) \( (i = 1, \ldots, n) \) satisfy the following globally Lipschitz condition

\[
\begin{align*}
|f_i(x_1, x_2, \ldots, x_i) - f_i(\hat{x}_1, \hat{x}_2, \ldots, \hat{x}_i)| \\
&\leq l(|x_1 - \hat{x}_1| + |x_2 - \hat{x}_2| + \cdots + |x_i - \hat{x}_i|),
\end{align*}
\]

(2)

where \( l \) is a positive constant.

There are some results on observer design for (1) without sampled and time delayed measurements, for example, (Deza and Busvelle [1992], Raff et al [2008]), the observers for Lipschitz nonlinear continuous time systems with nonuniformly sampled measurements are designed based on LMI and sampled data control techniques. In (Ahmed-Ali and Lamnabhi-Lagarrigue [2012]), some conditions on the maximum allowable transmission interval are given to guarantee an exponential convergence of the observation error for networked control systems. The authors proposed a sampled-data nonlinear observer design by using a continuous-time design coupled with an inter-sample output predictor (Karafyllis and Kravaris [2009]). In (Nadri et al [2013]), the problem of observer design was investigated for uniformly observable systems with sampled output measurements. There are some results on observer design for nonlinear uniformly observable systems with time-varying delayed output measurement (Van Assche et al [2011], Ahmed-Ali et al [2013a,b]). For example, in (Ahmed-Ali et al [2013b]), the authors addressed two classes of global exponential observers of continuous systems with sampled and delayed output measurements. There are two parts: a prediction part and a correction part. Sufficient conditions on the maximum allowable delay and the maximum allowable sampling period are also given to ensure exponential stability of the observation error.

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269
In this paper, we consider high gain observer design for the system (1) with sampled and delayed measurements. The observer is continuous and hybrid. By using an auxiliary integral technique, sufficient conditions are presented to ensure the global exponential stability of the observation error. Compared with the existing results, the systems we considered are more general, and the design method is simpler.

This paper is organized as follows. In Section 2, we present our main results: the continuous observer is designed for nonlinear systems with sampled and delayed output measurements. In Section 3, two examples are used to illustrate the validity of the proposed design method. Finally, the paper is concluded in Section 4.

2. CONTINUOUS OBSERVER DESIGN FOR THE SYSTEM (1)

We will design a continuous observer for the system (1), and present the upper bound of the maximum allowable sample period and the delay, so that the observation errors are globally exponentially convergent. The following lemma is useful for our main results.

Lemma 1. (Liu et al [2006]) For any positive definite matrix $M \in \mathbb{R}^{n \times n}$, scalar $\gamma > 0$, vector function $\omega : [0, \gamma] \rightarrow \mathbb{R}^n$ such that the integrations concerned are well defined, the following inequality holds:

$$
\int_0^\gamma w(s)ds \leq \gamma \int_0^\gamma \left( w(s)^\top M w(s) \right) ds.
$$

For the system (1), we design the following observer,

$$
\dot{x}_1(t) = \dot{x}_2(t) + L_1 e_1(t_k) + f_1(\dot{x}_1(t)),
\dot{x}_2(t) = \dot{x}_3(t) + L_2^2 e_2(t_k) + f_2(\dot{x}_1(t), \dot{x}_2(t)),
\dot{x}_n(t) = L_n^a e_n(t_k) + f_n(\dot{x}_1(t), \dot{x}_2(t), \ldots, \dot{x}_{n-1}(t)),
$$

where $L \geq 1$ is a constant, $e_i(t_k) = x_i(t_k) - \hat{x}_i(t_k)$, $a_i > 0$ $(i = 1, \ldots, n)$ are given such that there exists a symmetric positive definite matrix $P$ such that

$$
A^\top P + PA \leq -I,
$$

where $A = \begin{bmatrix} -a_1 & 1 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a_{n-1} & 0 & 0 & \cdots & 1 \\ -a_n & 0 & 0 & \cdots & 0 \end{bmatrix}$.

Note that $e_i(t_k)$ is a constant on $[t_k + \tau_k, t_k + T + \tau_{k+1})$ for $k \geq 0$ and $f_i(\cdot)$ $(i = 1, \ldots, n)$ are continuous and satisfy the condition (2), then, $\lim_{t \rightarrow t_k + T + \tau_{k+1}} \dot{x}_i(t) = \lim_{t \rightarrow t_k + T + \tau_{k+1}} \dot{x}_i(t)$ $(i = 1, \ldots, n)$. Therefore, $\dot{x}_i(t)$ $(i = 1, \ldots, n)$ are continuous on $[t_0, \infty)$.

Remark 1. Note that the state estimate is described in continuous time while the evolution process $x_i(t_k) - \hat{x}_i(t_k)$ is only updated at time instants $t_k + \tau_k$, that is, the current evolution process is used until the new evolution process is available. Therefore, the dynamics of observer (3) is of continuous and of hybrid nature.

Remark 2. Even though $\tau_k$ and $\tau_{k+1}$ are unknown, $e_i(t_k)$ is updated automatically in the observer whenever sampled and delayed measurement arrives. In [Ahmed-Ali et al [2013b]], the sampled and delayed measurement is available at instant $t_k + \tau_k$, however, $e_i(t_k)$ is updated at instant $t_k + \tau$, that is, there exists time delay $\tau - \tau_k$.

Remark 3. In this paper, the sampling period $T$ and the maximum allowable delay $\tau$ depend on the Observer (3).

From (1)-(3), for $k \geq 0$, we obtain the observation error:

$$
\begin{cases}
\dot{e}_1(t) = e_2(t) - L_1 e_1(t_k) + \tilde{f}_1, \\
\dot{e}_2(t) = e_3(t) - L_2^2 a_2 e_1(t_k) + \tilde{f}_2, \\
\vdots \\
\dot{e}_{n-1}(t) = e_n(t) - L_{n-1} a_{n-1} e_1(t_k) + \tilde{f}_{n-1}, \\
\dot{e}_n(t) = -L_n a_n e_1(t_k) + \tilde{f}_n, \\
t \in [t_k + \tau_k, t_k + T + \tau_{k+1}),
\end{cases}
$$

where $e_i(t) = x_i(t) - \hat{x}_i(t)$, $\tilde{f}_i = f_i(x_1(t), x_2(t), \ldots, x_i(t)) - f_i(\hat{x}_1(t), \hat{x}_2(t), \ldots, \hat{x}_i(t))$, $1 \leq i \leq n$.

Consider the following change of coordinates

$$
\epsilon_i(t) = \frac{e_i(t)}{L_i e_1(t_k)^{\frac{1}{2}}}, \quad i = 1, 2, \ldots, n,
$$

where $b$ is a positive real number. Then, we have

$$
\begin{cases}
\dot{\epsilon}_1(t) = \epsilon_2(t) - L_1 \epsilon_1(t_k) + \frac{\tilde{f}_1}{L_1^{b}}, \\
\dot{\epsilon}_2(t) = \epsilon_3(t) - L_2^2 a_2 \epsilon_1(t_k) + \frac{\tilde{f}_2}{L_1^{b}}, \\
\vdots \\
\dot{\epsilon}_{n-1}(t) = \epsilon_n(t) - L_{n-1} a_{n-1} \epsilon_1(t_k) + \frac{\tilde{f}_{n-1}}{L_1^{b}}, \\
\dot{\epsilon}_n(t) = -L_n a_n \epsilon_1(t_k) + \frac{\tilde{f}_n}{L_1^{b}}, \\
t \in [t_k + \tau_k, t_k + T + \tau_{k+1}].
\end{cases}
$$

Further, (7) can be rewritten as follows:

$$
\begin{cases}
\dot{\epsilon}_1(t) = \epsilon_2(t) - L_1 \epsilon_1(t_k) + \frac{\tilde{f}_1}{L_1^{b}}, \\
\dot{\epsilon}_2(t) = \epsilon_3(t) - L_2 a_2 \epsilon_1(t_k) + \frac{\tilde{f}_2}{L_1^{b+1}}, \\
\vdots \\
\dot{\epsilon}_{n-1}(t) = \epsilon_n(t) - L_{n-1} a_{n-1} \epsilon_1(t_k) + \frac{\tilde{f}_{n-1}}{L_1^{b+1}}, \\
\dot{\epsilon}_n(t) = -L_n a_n \epsilon_1(t_k) + \frac{\tilde{f}_n}{L_1^{b+1}}, \\
t \in [t_k + \tau_k, t_k + T + \tau_{k+1}].
\end{cases}
$$

Now, we will give our main results.

Theorem 1. Consider the system (1) with the condition (2). The output $y(t)$ is assumed to be sampled at instants $t_k$ and is available for the observer at instants $t_k + \tau_k$. Then, the state estimate $\hat{x}_i(t_k)$ is stable in continuous time and the estimation error $e_i(t_k)$ is stable in a hybrid nature.
Let $T = \frac{\kappa_1}{\lambda_1}$, $\bar{\tau} = \frac{\kappa_2}{\lambda_2}$ ($\kappa_1 > \kappa_2 > 0$ are two positive constants). If, $a_i > 0$ ($i = 1, \cdots, n$) are selected such that the condition (4) holds, and $L \geq 1$ is given such that $T + \bar{\tau}$ satisfies

$$T + \bar{\tau} \leq \min \left\{ \frac{L - 2\lambda_1 \hat{\rho}}{L}, \frac{1}{12nL^2 \bar{a}_i \bar{p}_2 + \hat{\rho}}, \frac{\rho \lambda_2}{12nL^3 \bar{a}_i^2} \right\},$$

then, the state observation error system (5) is globally exponentially stable, where $\bar{p}_2 = \lambda^{\max} (P^T \tilde{P})$, $\bar{a}_i = \max \{a_i^2\}$, $\lambda_1 = \lambda^{\max} (P)$, $\lambda_2 = \lambda^{\min} (P)$, $\hat{\rho} = \sqrt{\frac{\nu - 1}{2\lambda_1}}$.

**Proof:** Consider the positive definite function

$$V_1(t) = \varepsilon(t)^T P \varepsilon(t), \quad (10)$$

where $\varepsilon(t) = [\varepsilon_1(t), \cdots, \varepsilon_n(t)]^T$, then the derivative of $V_1(t)$ along the system (8) is given as follows:

$$\frac{d}{dt} V_1(t)_{|\varepsilon(t)} = \varepsilon(t)^T P \varepsilon(t) + \varepsilon(t)^T P \tilde{P} \varepsilon(t)$$

$$\leq -L \varepsilon(t)^T \varepsilon(t) + 2 \sum_{i=1}^{n} \sum_{j=1}^{n} | \varepsilon_i(t) P_{ij} |$$

$$\times |L^b \varepsilon_1(t) - 1| + |L^{1+b} \varepsilon_2(t) + \cdots + |L^{1+b} \varepsilon_n(t) - 1|$$

$$+ 2L \varepsilon(t)^T P \begin{pmatrix} a_1(\varepsilon_1(t) - \varepsilon_1(t_k)) \\ \vdots \\ a_n(\varepsilon_n(t) - \varepsilon_n(t_k)) \end{pmatrix}$$

$$\leq (-\frac{3}{4} - 2n\bar{p}_1 I) \varepsilon(t)^T \varepsilon(t) + 4Ln \bar{a}_i \bar{p}_2 (\varepsilon_1(t) - \varepsilon_1(t_k))^2,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}], \quad (11)$$

where $P_{ij}$ is the element of $P$ at the $i$th line and $j$th column, $\bar{p}_1 = \max \{|P_{ij}|\}$.

Note that there exists $L_1 > 1$ such that $L > 8n\bar{p}_1 I$, for $L > L_1$. Then,

$$\frac{d}{dt} V_1(t)_{|\varepsilon(t)} \leq -\frac{1}{2} L \varepsilon(t)^T \varepsilon(t) + 4nL \bar{a}_i \bar{p}_2 (\varepsilon_1(t) - \varepsilon_1(t_k))^2,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}]. \quad (12)$$

By Lemma 1, we have

$$| \varepsilon_1(t) - \varepsilon_1(t_k) |^2 = \int_{t_k}^{t} \varepsilon_1(s)^2 ds \leq (t - t_k)$$

$$\times \int_{t_k}^{t} | \varepsilon_1(s) |^2 ds \leq L(t - t_k) \int_{t_k}^{t} | \varepsilon_2(s) - a_1 \varepsilon_1(t_k) + \varepsilon_1(t_k) |^2 ds$$

$$\leq 3(t - t_k) L^2 \int_{t_k}^{t} | \varepsilon_2(s) |^2 + \int_{t_k}^{t} \varepsilon_1(t_k)^2 ds,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}]. \quad (13)$$

Then, there exists $L_2 > 1$ such that when $L > L_2$, we have $L^{b+1} > l$.

If follows from (12) and (13) that

$$\frac{d}{dt} V_1(t)_{|\varepsilon(t)} \leq -\frac{1}{2} L \varepsilon(t)^T \varepsilon(t) + 12nL^3 \bar{a}_i^2 \bar{p}_2 (t - t_k)^2 \varepsilon_1(t_k)^2$$

$$+ 12nL^3 \bar{a}_i \varepsilon_2(t - t_k) \int_{t_k}^{t} | \varepsilon_1(s)^2 | ds,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}].$$

Note that when $t \in [t_k + \tau_k, t_k + T + \tau_{k+1}]$, we have $t - t_k - \tau_k < T + \tau_{k+1} - \tau_k$, that is, $t - T + \tau_{k+1} < t_k$. Then,

$$\frac{d}{dt} V_2(t) \leq -\frac{1}{2} L \varepsilon(t)^T \varepsilon(t) + 12nL^3 \bar{a}_i^2 \bar{p}_2 (t - t_k)^2 \varepsilon_1(t_k)^2$$

$$+ 12nL^3 \bar{a}_i \varepsilon_2(t - t_k) \int_{t - T + \tau_{k+1}}^{t} | \varepsilon_1(s)^2 | ds,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}]. \quad (14)$$

Construct the following auxiliary integral function

$$V_2(t) = \int_{t - T + \tau_{k+1}}^{t} | \varepsilon_1(s)^2 | ds,$$

$$t \in [t_k, \infty), \quad (15)$$

where $k_0 = \min \{k : T + \tau < t_k\}$. Then,

$$\frac{d}{dt} V_2(t) = (T + \tau) | \varepsilon_1(t)^2 | + \varepsilon_2(t)^2 + \cdots + \varepsilon_n(t)^2$$

$$- \int_{t - T + \tau_{k+1}}^{t} | \varepsilon_1(s)^2 | ds.$$ \quad (16)

Now, we consider the following Lyapunov-Krasovskii function

$$V(t) = V_1(t) + LV_2(t). \quad (17)$$

Calculate the derivative of $V(t)$ defined in (17) along the system (8), we have

$$\frac{d}{dt} V(t)_{|\varepsilon(t)} \leq -\left( \frac{1}{2} + (T + \tau) \right) L \varepsilon(t)^T \varepsilon(t) + 12nL^3 \bar{a}_i^2 \bar{p}_2$$

$$(T + \tau) \varepsilon_1(t_k)^2 + (12nL^3 \bar{a}_i \bar{p}_2 (T + \tau) - 1) L \varepsilon_1(t_k)^2$$

$$+ \varepsilon_2(t)^2 + \cdots + \varepsilon_n(t)^2 ds,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}], \quad k \geq k_0. \quad (18)$$

Note that

$$V_2(t) \leq (T + \tau) \int_{t - T + \tau_{k+1}}^{t} | \varepsilon_1(s)^2 | ds,$$

$$t \in [t_k + \tau_k, t_k + T + \tau_{k+1}]. \quad (19)$$
Thus, (18) and (19) imply
\[
\begin{align*}
\frac{d}{dt}V(t)|_{(8)} &\leq -\left(\frac{1}{2} - (T + \bar{\tau})\right)L\varepsilon(t)^{\top}\varepsilon(t) \\
&- \frac{1 - 12L^2n\hat{a}_1p_2(T + \bar{\tau})^2}{(T + \bar{\tau})}LV_2(t) + 12nL^3\hat{a}_1^2p_2(T + \bar{\tau})^2 \\
&\times \varepsilon_1(t_k)^2 \\
&- \frac{1}{2\lambda_1}(1 - (T + \bar{\tau}))LV_1(t) + \frac{12nL^3\hat{a}_1^2p_2(T + \bar{\tau})^2}{\lambda_2}V_1(t_k),
\end{align*}
\]
\(t \in [t_k + \tau_k, t_k + T + \tau_{k+1}], \ k \geq k_0.
\tag{20}
\]
Since \(T + \tau\) satisfies (9), then, we have
\[
\begin{align*}
\frac{d}{dt}V(t)|_{(8)} &\leq -\hat{\rho}V(t) + (T + \bar{\tau})\hat{\rho}V(t_k), \\
&\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \ k \geq k_0.
\end{align*}
\tag{21}
\]
From the above differential inequality, we obtain
\[
V(t) \leq e^{-\hat{\rho}(t-t_k-\tau_k)}V(t_k + \tau_k) + (T + \bar{\tau})V(t_k) \\
- (T + \bar{\tau})e^{-\hat{\rho}(t-t_k-\tau_k)}V(t_k), \\
\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \ k \geq k_0.
\]
Let \(t = t_k + T + \tau_{k+1}\) and \(t = t_k + T,\) respectively, we have
\[
\begin{align*}
V(t_k + T + \tau_{k+1}) &\leq e^{-\hat{\rho}(T+t_k-\tau_k)}V(t_k + \tau_k) \\
&+ (T + \bar{\tau})V(t_k) - (T + \bar{\tau})e^{-\hat{\rho}(T+t_k-\tau_k)}V(t_k),
\end{align*}
\]
and,
\[
V(t_k + T) \leq e^{-\hat{\rho}(T-\tau_k)}V(t_k + \tau_k) + (T + \bar{\tau})V(t_k) \\
- (T + \bar{\tau})e^{-\hat{\rho}(T-\tau_k)}V(t_k).
\]
Thus,
\[
\begin{align*}
V(t_k + T + \tau_{k+1}) + \rho V(t_k + T) \\
\leq e^{-\hat{\rho}(T-\tau)}(1 + \rho)V(t_k + \tau_k) + 2(T + \bar{\tau})V(t_k),
\end{align*}
\tag{22}
\]
where \(0 < \rho < 1\) is a positive constant and will be determined later. Note that \(T = \frac{\bar{\tau}}{2},\ \bar{\tau} = \frac{\bar{\tau}}{2} (\kappa_1 > \kappa_2),\) and \(\hat{\rho} = \frac{\sqrt{L} - 1}{2\lambda_1},\) then, there exists \(L_3 > 1\) such that when \(L > L_3,\) we have
\[
2(\kappa_1 + \kappa_2) \leq \frac{(\sqrt{L} - 1)(\kappa_1 - \kappa_2)}{2\lambda_1}.
\]
Since
\[
\hat{\rho}(\kappa_1 - \kappa_2) = \frac{(\sqrt{L} - 1)(\kappa_1 - \kappa_2)}{2\lambda_1},
\]
and
\[
e^{\hat{\rho}(\kappa_1 - \kappa_2)/L^3} > 1 + \hat{\rho}(\kappa_1 - \kappa_2)/L^3,
\]
then,
\[
2(\kappa_1 + \kappa_2)/L^3 < \hat{\rho}(\kappa_1 - \kappa_2)/L^3 < e^{\hat{\rho}(\kappa_1 - \kappa_2)/L^3} - 1.
\]
Therefore, there exist \(L_4 > 1, 0 < \rho < 1\) such that
\[
2(\kappa_1 + \kappa_2)/L^3 < \rho < e^{\hat{\rho}(\kappa_1 - \kappa_2)/L^3} - 1,
\]
for \(L > L_4.\) Thus,
\[
e^{-\hat{\rho}(T-\tau)}(1 + \rho) < 1, 2(T + \bar{\tau}) < \rho
\tag{23}
\]
Therefore, we can select \(L > \max\{L_1, L_2, L_3, L_4\}\) such that
\[
\eta = \max\{e^{-\hat{\rho}(T-\tau)}(1 + \rho), \frac{2(T + \bar{\tau})}{\rho}\} < 1.
\]
Therefore, it follows from (22) that
\[
\begin{align*}
V(t_k + \tau_k + \bar{\tau}_k + 1) + \rho V(t_k + T) \\
= V(t_k + T + \tau_k + 1) + \rho V(t_k + T) \\
\leq \eta[V(t_k + \tau_k) + \rho V(t_k)], \ k \geq k_0.
\end{align*}
\tag{24}
\]
Applying iteratively (24), for \(k \geq k_0,\) we have
\[
V(t_k + \tau_k) + \rho V(t_k) \leq \eta^{k-k_0}[V(t_{k_0} + \tau_{k_0}) + \rho V(t_{k_0})]
\tag{25}
\]
It follows from (21) and (25) that
\[
\begin{align*}
V(t_k + \tau_k) + \rho V(t_k) \\
\leq \eta^{k-k_0}[V(t_{k_0} + \tau_{k_0}) + \rho V(t_{k_0})], \\
\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \ k \geq k_0.
\end{align*}
\tag{26}
\]
For any \(t > t_{k_0} + \tau_{k_0},\) there exists \(k \geq k_0\) such that \(t \in [t_k + \tau_k, t_k + T + \tau_{k+1}].\) Note that \(t - t_{k_0} - \tau_{k_0} - 1 \leq k \leq t - t_{k_0} - \tau_{k_0}.\) Then,
\[
\begin{align*}
V(t) &\leq \eta^{t-t_{k_0}-\tau_{k_0}-1}[V(t_{k_0} + \tau_{k_0}) + \rho V(t_{k_0})] \\
&= \eta^t \eta^{t-t_{k_0}-\tau_{k_0}-1}[V(t_{k_0} + \tau_{k_0}) + \rho V(t_{k_0})], \\
\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \ k \geq k_0.
\end{align*}
\tag{26}
\]
That is, the system (8) is globally exponentially stable.

Remark 4. The value of \(\eta\) has an effect on the convergent time. The state observation error has a faster convergent speed with a smaller value of \(\eta.\) A large value of \(L\) can be selected to make \(\eta\) small. However, it may yield a small sampling period \(T.\) In practical application, we can select a proper \(L\) (on \(T\) and \(\bar{\tau}\)) to achieve the desired effect.

Remark 5. The change of coordinates (6) differs by the positive real number \(b\) from the standard change of coordinates used in high-gain observers where \(b = 0.\) If the lipschitz constant \(l\) is very large, we can choose a proper constant \(b\) such that \(L\) is not very large. Then, the parameter \(b\) gives more flexibility on selection of the high gain \(L.\)

3. Example and Simulation

In this section, we use two examples to show the effectiveness of our high gain observer design for nonlinear systems with sampled and delayed measurements.

Example 1. An academic bioreactor is reactor in which microorganisms grow by eating a substrate. Let \(x_1(t)\) and \(x_2(t)\) denote the concentrations of microorganisms and substrate, respectively. Then, the following standard equations for the bioreactor (Contois [1959]) can be obtained:
\[
\begin{align*}
\dot{x}_1(t) &= \frac{a_1x_1(t)x_2(t)}{a_2x_1(t) + x_2(t)} - u(t)x_1(t), \\
\dot{x}_2(t) &= -\frac{a_2x_1(t)x_2(t)}{a_2x_1(t) + x_2(t)} - u(t)x_2(t) + u(t)a_4, \\
y(t) &= x_1(t),
\end{align*}
\tag{27}
\]

where the control $u(t)$ is in the interval $\Theta_u = \left[u_{\min}, u_{\max}\right] \subset (0, 1)$ and we choose $a_1 = a_2 = a_3 = 1, a_4 = 0.1$.
In (Gauthier et al [1992]), it is observed that the set $\Theta_u' = (x_1(t), x_2(t)) \in \mathbb{R}^2 : x_1(t) \geq \gamma_1, x_2(t) \geq \gamma_2, x_1(t) + x_2(t) \leq 1$ is forward invariant, where $\gamma_1 = (1 - u_{\max}/u_{\max})$ and $u_{\min} = \gamma_2 / (0.1 - \gamma_2)$. This means that the bioreactor state solutions are bounded and actually remain in a known compact set. After the state transformation $x_1(t) = x'_1(t), x_2(t) = x_1(t)x_2(t)/(x'_1(t) + x'_2(t))$, we have

$$\begin{align*}
\dot{x}_1(t) &= x_2(t) - u(t)x_1(t), \\
\dot{x}_2(t) &= -x_2(t)u(t).
\end{align*}$$

We get the following equation for the observer:

$$\begin{align*}
\dot{\hat{x}}_1(t) &= \hat{x}_2(t) - u(t)\hat{x}_1(t) + 3L(y(t_k) - \hat{x}_1(t_k)), \\
\dot{\hat{x}}_2(t) &= \frac{x_3(t) + x_2(t)^2(0.1u(t) - x_2(t))}{x_1(t)} \\
&\quad - x_2(t)u(t) + 2L^2(y(t_k) - \hat{x}_1(t_k)), \\
t &\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \quad k \geq 0.
\end{align*}$$

In the following simulation, we apply the input $u(t) = 0.08$, for $t \leq 10$, $u(t) = 0.02$, for $10 < t$, $x_0 = [0.7, 0.3]^T$, $\hat{x}_0 = [0.2, 0.5]^T$, $L = 1$, the sampling period $T = 0.1s$ and the delay $\tau_k$ satisfying $0 \leq \tau_k \leq 0.05s$. The trajectories of the error states are shown in Fig. 1. In practice, the measure is often disturbed by a white noise. Fig. 2 also shows the trajectories of the errors with white noise.

![Fig. 1 Trajectories of the errors $e_1(t)$ and $e_2(t)$](image1)

![Fig. 2 Trajectories of the errors $e_1(t)$ and $e_2(t)$ with white noise.](image2)

**Example 2.** A single-link robot arm system can be modeled by (Isidori [1995]) or (Marino and Tomei [1995])

$$\begin{align*}
\dot{z}_1(t) &= z_2(t), \\
\dot{z}_2(t) &= \frac{K}{J_2N^2}z_3(t) - \frac{F_1(t)}{J_1} - \frac{K}{J_2}z_2(t) - \frac{mgd}{J_2z_2(t)} - \frac{mgd}{J_2}(\cos(z_1(t))) - \frac{mgd}{J_2}(\cos(z_1(t))) - 1, \\
\dot{z}_3(t) &= z_4(t), \\
\dot{z}_4(t) &= \frac{1}{J_1}u(t) + \frac{K}{J_1N}z_1(t) - \frac{K}{J_2N}z_3(t) - \frac{F_1(t)}{J_1}z_4(t), \\
y(t) &= z_1(t),
\end{align*}$$

where $J_1, J_2, K, N, m, g, d$ are known parameters, $F_1(t)$ and $F_2(t)$ are viscous friction coefficients that are not precisely known. Suppose $F_1(t)$ and $F_2(t)$ are bounded by an unknown constant $C > 0$. Consider the change of coordinates

$$\begin{align*}
x_1(t) &= z_1(t), \quad x_2(t) = z_2(t), \\
x_3(t) &= \frac{K}{J_2N}z_3(t) - \frac{mgd}{J_2z_2(t)}, \quad x_4(t) = \frac{K}{J_2N}z_4(t)
\end{align*}$$

and the pre-feedback

$$v = \frac{K}{J_1N} \left(1 - \frac{mgd}{J_2z_2(t)}\right),$$

which transforms (28) into

$$\begin{align*}
\dot{\hat{x}}_1(t) &= x_2(t), \\
\dot{\hat{x}}_2(t) &= x_3(t) - \frac{F_1(t)}{J_1} - \frac{K}{J_2}x_1(t) - \frac{mgd}{J_2}(\cos(x_1(t))) - 1, \\
\dot{\hat{x}}_3(t) &= x_4(t), \\
\dot{\hat{x}}_4(t) &= v + \frac{K^2}{J_1J_2N^2}x_1(t) - \frac{F_1(t)}{J_1} - \frac{K}{J_2N}x_3(t) - \frac{F_1(t)}{J_1}x_4(t), \\
y(t) &= x_1(t).
\end{align*}$$

Construct the following observer:

$$\begin{align*}
\dot{\hat{x}}_1(t) &= \hat{x}_2(t) + 4L(y(t_k) - \hat{x}_1(t_k)), \\
\dot{\hat{x}}_2(t) &= \hat{x}_3(t) - \frac{F_1(t)}{J_1} - \frac{K}{J_2}x_1(t) - \frac{mgd}{J_2}(\cos(\hat{x}_1(t))) - 1 + 6L^2(y(t_k) - \hat{x}_1(t_k)), \\
\dot{\hat{x}}_3(t) &= \hat{x}_4(t) + 4L^3(y(t_k) - \hat{x}_1(t_k)), \\
\dot{\hat{x}}_4(t) &= v + \frac{K^2}{J_1J_2N^2}x_1(t) - \frac{F_1(t)}{J_1} - \frac{K}{J_2N}x_3(t) - \frac{F_1(t)}{J_1}x_4(t) + L^2(y(t_k) - \hat{x}_1(t_k)), \\
t &\in [t_k + \tau_k, t_k + T + \tau_{k+1}], \quad k \geq 0.
\end{align*}$$

In the following simulation, we apply the system parameters: $K/J_2 = 5, mgd/J_2 = 4, K^2/(J_1J_2N^2) = 2, K/(J_1N) = 3$. The initial conditions of the whole system are $(x_1(0), x_2(0), x_3(0), x_4(0)) = (-5, -1, 4, 2)$ and $(\hat{x}_1(0), \hat{x}_2(0), \hat{x}_3(0), \hat{x}_4(0)) = (5, 3, -1, -4), a = (4, 6, 4, 1)^T$, and $L = 1$. The sampling period $T$ and the delay $\tau_k$ are chosen as $T = 0.1s$ and $0 \leq \tau_k \leq 0.05s$. The simulation results is shown in Fig. 3. In practice, the measure may be disturbed by a white noise. The trajectories of the errors with white noise are also shown in Fig. 4.
4. CONCLUSION

In this paper, we designed observers for nonlinear systems with sampled and delayed output measurements. The observers were continuous and hybrid in nature. Based on an auxiliary integral technique, the exponential stability of the estimation errors was achieved, and the sampling period and the maximum delay were also given. Finally, numerical examples were provided to illustrate the design methods.

REFERENCES


